



*Engineering, LLC*

**PROJECT NARRATIVE  
AND  
STORM DRAINAGE ANALYSIS**

**FOR**

**ARLINGTON HEIGHTS INDUSTRIAL  
703-723 ALGONQUIN ROAD  
ARLINGTON HEIGHTS, IL**

PREPARED FOR:

**MORGAN/HARBOUR CONSTRUCTION LLC  
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**JOB# 322-127-17-301**

OCTOBER 18, 2017

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October 18, 2017

File: 322-127-17

Arlington Heights Industrial

703-723 Algonquin Road  
Arlington Heights, IL  
15.41 Acre Property

Narrative Description of Proposed Development

(Refer Also to Final Engineering Plans, Notes and Exhibits.)

**General:**

The subject parcel is located southeasterly of Algonquin Road and Meijer Drive in Arlington Heights, Illinois. The Jane Adams Memorial Tollway (I-90) is along the southern boundary of the property. Currently, two light industrial/office buildings are on the site. The northern building is on existing Parcel 1, which consists of 7.04 acres. The southern building is on existing Parcel 2, which consists of 8.37 acres. The proposed improvements include one building of approximately 331,000 sq ft for warehousing/distribution. Construction is to proceed in two phases. The first phase would be on existing Parcel 1, during which time the existing building on Parcel 2 would remain operational. With the Phase 2 improvements, the Phase 1 building would extend into the Parcel 2 area. Since the site currently consists of two parcels, a Plat of Subdivision combining the site into one lot is proposed.

**Stormwater Management:**

The existing Parcel 1 drains to the north with a storm drain connection at the northeast corner of the parcel to the existing 18" storm sewer along the southerly side of Algonquin Road. Storm water discharge from the site is controlled by an existing 4" PVC pipe, as well as a secondary 10" RCP pipe at a higher elevation. The existing overland flow from Parcel 1 to Algonquin Rd is within the easterly driveway at an approximate elevation of 715.43. No improvements to this existing driveway are proposed within the Algonquin Rd right-of-way. Therefore, for design purposes an overflow elevation of 715.4 is used. At the 715.4 elevation, the existing 4" PVC has a release of approximately 0.69 cfs and the 10" RCP has a release of 4.44 cfs, for a total of 5.13 cfs.

The existing Parcel 2 drains to the south, via an existing 18" RCP pipe, which connects to an existing 36" storm sewer with discharge to an open waterway along the north side of I-90. No restrictor was located within the existing 18" RCP storm sewer. The existing overland flow from parcel 2 is to the south at an approximate elevation of 715.0. At this 715.0 overflow elevation, the existing release thru the 18" RCP is approximately 21.17". Since there is no offsite area tributary to Parcel 2 which would be impacted by a slight rise in the overflow elevation, a 715.4 high water level (HWL)/overflow elevation is used for both the Phase 1 and Phase 2 site improvements.

Stormwater detention requirements were reviewed for both the Village of Arlington Heights, and the Metropolitan Water Reclamation District of Greater Chicago (MWRD) criteria. Also, the MWRD volume control requirements were reviewed. Since there are some slight deviations in the Phase 2 improvements draining to the north from the proposed site improvements with Phase 1, both conditions were reviewed. In consideration of the worst case scenario, the proposed design implements the more restrictive criteria. A Drainage Summary Sheet, Table 1, is attached which provides a summary of the allowable release rate, as well as the detention, and volume control requirements for the various scenarios.

For the north drainage area in the proposed condition, the existing 4" PVC is to remain, and a 3-1/8" orifice plate is to be provided in the existing 10" RCP. This results in a total release of 1.21 cfs at the 715.4 elevation. For the south drainage area, a 5" orifice plate is proposed for the 18" RCP, restricting the release to 1.53 cfs at the 714.4 HWL.

The detention volumes associated with the above design release rates were reviewed. Per the attached calculations, using these design release rates, the detention storage volume for the north area would be 2.69 ac-ft, and 3.16 ac-ft for the south, phase 2 area.

A Summary of Storage Provided, Table 2, is attached outlining the storage volumes provided in the respective basins and locations. Although, there may be some minor refinement of allocations between detention and volume control storage in the underground basins, the total volumes provided are appropriate based on both the Village of Arlington Heights and the MWRD criteria. As noted, stormwater storage is provided in a combination of areas, including vegetated/open water basins, underground storage, pipe storage, and surface ponding in the truck dock areas. It is noted the ponding in the truck dock areas will occur during the more intense storms only, with the proposed rims at a 714.05 elevation. Therefore, at the upper elevations of the detention storage system, a maximum water depth of 1.35' would be expected at the 715.4 HWL/overflow elevation.

TABLE 1--ARLINGTON HEIGHTS INDUSTRIAL - DRAINAGE SUMMARY SHEET

## VILLAGE OF ARLINGTON HEIGHTS CRITERIA:

Temp. DRAINAGE AREA (ac.)	Offsite DRAINAGE AREA (ac.)	Temp./TOTAL AREA (ac.)	DRAINAGE AREA (ac.)	Offsite DRAINAGE AREA (ac.)	TOTAL AREA (ac.)	IMPERVIOUS AREA (ac.) onsite only	IMPERVIOUS AREA (ac.) Total w/ offsite	% Impervious	COMPOSITE "C"	ALLOWABLE RELEASE (cfs)	Detention Required (ac- ft)
7.04	0.396	7.436			5.843	5.902	80%	0.86	1.33	2.60	
			6.875	0.396	6.934	5.957	6.016	87%	0.89	1.24	2.55
			8.540	0.016	8.556	7.498	7.514	88%	0.90	1.54	3.16

MWRD CRITERIA:

## MWRD VOLUME CONTROL:

**PHASE 1** (full build out-max impervious)  
1" of voli  
OME CONTROL.

1" of volume over total impervious area of -----

1" of volume over total impervious area of -----

**Required Volume =** 0.50 Ac-Ft

# RESTRICTIVE CULVERT WORKSHEET

## JOB DATA:

Job Name:	<u>ALGONQUIN RD IBDUSTRIAL-PH 1</u>
Job Number:	<u>322-127-17</u>
Designer:	<u>PDL</u>
Description	<u>EXIST STORM OUTFALL-4" PRIMARY</u>

FLOWS ARE BASED ON THE FOLLOWING EQUATION:

$$Q = A \sqrt{\frac{H}{\frac{K_e + K_o}{2g} + \frac{2.87(n)^2 L}{\sqrt[3]{\phi^4}}}}$$

Q = FLOW (cfs)

A = AREA (sqr.ft.)

H = Head (ft.)

K<sub>e</sub> & K<sub>o</sub> = Entrance & Outlet Loss Coefficients

n = Manning's Roughness Coeficent

g = 32.2 ft/sec<sup>2</sup>

= diameter

$\phi$

## PIPE DATA:

Pipe Diameter (feet)	<b>0.33</b>	ft.
Pipe Area (sqr. ft)	0.087	sqr. ft.
Slope (ft./ft.)	<b>-0.0023</b>	
Length of Pipe (ft.)	<b>30</b>	ft.
Existing Invert Elevation	<b>709.67</b>	ft.
Backwater Elevation	<b>710.07</b>	ft. (Top of 4" pipe @ outlet)
Manning's "n" value	<b>0.013</b>	
Entrance Loss Coefficient	<b>0.50</b>	
Outlet Loss Coefficient	<b>1.00</b>	

## RATING TABLE:

Water Elevation (ft.)*	Head (ft.)	Q (cfs)
715.00	4.93	0.66
715.10	5.03	0.67
715.20	5.13	0.67
715.30	5.23	0.68
715.40	5.33	0.69
715.50	5.43	0.69
715.60	5.53	0.70
715.70	5.63	0.70
715.80	5.73	0.71
715.90	5.83	0.72
716.00	5.93	0.72

\*Water elevation must be higher than backwater elevation.

# RESTRICTIVE CULVERT WORKSHEET

## **JOB DATA:**

Job Name:	<u>ALGONQUIN RD IBDUSTRIAL-PH 1</u>
Job Number:	<u>322-127-17</u>
Designer:	<u>PDL</u>
Description	<u>EXIST STM OUTFALL-10" SECONDARY</u>

FLOWS ARE BASED ON THE FOLLOWING EQUATION:

$$Q = A \sqrt{\frac{H}{\frac{K_e + K_o}{2g} + \frac{2.87(n)^2 L}{\sqrt[3]{\phi^4}}}}$$

Q = FLOW (cfs)

A = AREA (sqr.ft.)

H = Head (ft.)

K<sub>e</sub> & K<sub>o</sub> = Entrance & Outlet Loss Coefficients

n = Manning's Roughness Coeficient

g = 32.2 ft/sec<sup>2</sup>

= diameter

$\phi$

## **PIPE DATA:**

Pipe Diameter (feet)	<b>0.83</b>	ft.
Pipe Area (sqr. ft)	0.541	sqr. ft.
Slope (ft./ft.)	<b>-0.021</b>	
Length of Pipe (ft.)	<b>30</b>	ft.
Existing Invert Elevation	<b>711.12</b>	ft.
Backwater Elevation	<b>712.58</b>	ft. (Ttop of 10" pipe @ outlet)
Manning's "n" value	<b>0.013</b>	
Entrance Loss Coefficient	<b>0.50</b>	
Outlet Loss Coefficient	<b>1.00</b>	

## **RATING TABLE:**

Water Elevation (ft.)*	Head (ft.)	Q (cfs)
715.00	2.42	4.11
715.10	2.52	4.19
715.20	2.62	4.28
715.30	2.72	4.36
715.40	2.82	4.44
715.50	2.92	4.51
715.60	3.02	4.59
715.70	3.12	4.67
715.80	3.22	4.74
715.90	3.32	4.81
716.00	3.42	4.89

\*Water elevation must be higher than backwater elevation.

# RESTRICTIVE CULVERT WORKSHEET

**JOB DATA:**

Job Name:	<u>ALGONQUIN RD IBDUSTRAL-PH 2</u>
Job Number:	<u>322-127-17</u>
Designer:	<u>PDL</u>
Description	<u>EXIST STM OUTFALL-18"</u>

FLOWS ARE BASED ON THE FOLLOWING EQUATION:

$$Q = A \sqrt{\frac{H}{\frac{K_e + K_o}{2g} + \frac{2.87(n)^2 L}{\sqrt[3]{\phi^4}}}}$$

Q = FLOW (cfs)

A = AREA (sqr.ft.)

H = Head (ft.)

K<sub>e</sub> & K<sub>o</sub> = Entrance & Outlet Loss Coefficients

n = Manning's Roughness Coeficient

g = 32.2 ft/sec<sup>2</sup>

= diameter

$\phi$

**PIPE DATA:**

Pipe Diameter (feet)	<u>1.50</u>	ft.
Pipe Area (sqr. ft)	<u>1.767</u>	sqr. ft.
Slope (ft./ft.)	<u>0</u>	ft.
Length of Pipe (ft.)	<u>10</u>	ft.
Existing Invert Elevation	<u>709.75</u>	ft.
Backwater Elevation	<u>711.25</u>	ft. (Top of 18" pipe)
Manning's "n" value	<u>0.013</u>	
Entrance Loss Coefficient	<u>0.50</u>	
Outlet Loss Coefficient	<u>1.00</u>	

**RATING TABLE:**

Water Elevation (ft.)*	Head (ft.)	Q (cfs)
714.60	3.35	20.01
714.70	3.45	20.31
714.80	3.55	20.60
714.90	3.65	20.89
715.00	3.75	21.17
715.10	3.85	21.45
715.20	3.95	21.73
715.30	4.05	22.00
715.40	4.15	22.27
715.50	4.25	22.54
715.60	4.35	22.80

\*Water elevation must be higher than backwater elevation.

# ORIFICE WORKSHEET

Job Name:	ALGONQUIN RD INDUSTRIAL-PH 1
Job Number:	322-127-17
Designer:	PDL
Description	PROPOSED ORIFICE IN EXIST 10" RCP

FLOWS ARE BASED ON THE FOLLOWING EQUATION:

$$Q = AC\sqrt{2gH}$$

Q = FLOW (cfs)  
A = AREA (sqr.ft.)  
C = Orifice Coefficient  
g = 32.2 ft/sec<sup>2</sup>  
H = Head (ft.)

## ORIFICE DATA:

Orifice diameter(inches)	3.125	inches
Orifice area(square feet)	0.053	sqr. ft.
Proposed invert elevation	711.12	ft.
Centerline of flow	711.25	ft
Orifice coefficient	0.6	

## RATING TABLE:

Water Elevation (ft.)*	Head (ft.)	Q (cfs)
715.00	3.75	0.50
715.10	3.85	0.50
715.20	3.95	0.51
715.30	4.05	0.52
715.40	4.15	0.52
715.50	4.25	0.53
715.60	4.35	0.53
715.70	4.45	0.54
715.80	4.55	0.55
715.90	4.65	0.55
716.00	4.75	0.56
716.10	4.85	0.56

\*Water elevation must be higher than centerline of flow

# ORIFICE WORKSHEET

Job Name:	ALGONQUIN RD INDUSTRIAL-PH 2
Job Number:	322-127-17
Designer:	PDL
Description	PROPOSED ORIFICE IN EXIST 18" RCP

FLOWS ARE BASED ON THE FOLLOWING EQUATION:

$$Q = AC\sqrt{2gH}$$

Q = FLOW (cfs)  
A = AREA (sqr.ft.)  
C = Orifice Coefficient  
g = 32.2 ft/sec<sup>2</sup>  
H = Head (ft.)

## ORIFICE DATA:

Orifice diameter(inches)	5.000	inches
Orifice area(square feet)	0.136	sqr. ft.
Proposed invert elevation	709.75	ft.
Centerline of flow	709.96	ft
Orifice coefficient	0.6	

## RATING TABLE:

Water Elevation (ft.)*	Head (ft.)	Q (cfs)
715.00	5.04	1.47
715.10	5.14	1.49
715.20	5.24	1.50
715.30	5.34	1.52
715.40	5.44	1.53
715.50	5.54	1.55
715.60	5.64	1.56
715.70	5.74	1.57
715.80	5.84	1.59
715.90	5.94	1.60
716.00	6.04	1.61
716.10	6.14	1.63

\*Water elevation must be higher than centerline of flow

**RWG ENGINEERING, LLC.**  
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**(630) 774-9501**

Detention Calculator  
Modified Rational Method

TELEPHONE (630) 774-9501			DESCRIPTION		Arlington Heights - BASIN CALCULATION SHEETS		
					Technical Bulletin 70 (7.58 in. - 100 Year Rainfall)		
					STORAGE VOLUME WITH ALLOWABLE RELEASE RATE-PHASE 1 TEMPORARY		
DURATION	TIME	100 YR. INT	INFLOW RATE	STORED RATE	VOLUME		
(HOURS)	(MIN)	(IN/HR)	(CFS)	(CFS)	(ACRE-FT)	Area of site in acres:	7.44
0.50	30	5.60	35.81	34.48	1.44	Trapped water area in acres:	0.00
0.67	40	4.92	31.46	30.13	1.67	Net area for release computation in acres:	0.00
0.83	50	4.24	27.11	25.78	1.79	Allowable release rate in CFS:	1.33
1.00	60	3.56	22.77	21.44	1.79	Unrestricted release rate in CFS:	0.00
1.50	90	2.90	18.55	17.22	2.15	Bypass release rate in CFS:	0.00
2.00	120	2.24	14.32	12.99	2.17	Total allowable release in CFS:	1.33
3.00	180	1.62	10.36	9.03	2.26	Developed runoff coefficient:	0.86
4.00	240	1.40	8.93	7.60	2.53		
5.00	300	1.17	7.50	6.17	2.57	Maximum volume in Acre-Ft =	2.60
6.00	360	0.95	6.08	4.75	2.37		
7.00	420	0.88	5.65	4.32	2.52		
8.00	480	0.82	5.22	3.89	2.60		
9.00	540	0.75	4.80	3.47	2.60 <====		
10.00	600	0.68	4.37	3.04	2.53		
11.00	660	0.62	3.94	2.61	2.40		
12.00	720	0.55	3.52	2.19	2.19		
13.00	780	0.52	3.35	2.02	2.18		
14.00	840	0.50	3.18	1.85	2.15		
15.00	900	0.47	3.01	1.68	2.09	Phase 1:	
16.00	960	0.44	2.84	1.51	2.01	Total Tributary Area after Phase 1 = 7.436 ac.	
17.00	1020	0.42	2.66	1.33	1.89	Release rate = 1.33 cfs	
18.00	1080	0.39	2.49	1.16	1.75		
19.00	1140	0.38	2.42	1.09	1.72		
20.00	1200	0.37	2.34	1.01	1.69		
21.00	1260	0.36	2.27	0.94	1.65		
22.00	1320	0.34	2.20	0.87	1.59		
23.00	1380	0.33	2.12	0.79	1.52		
24.00	1440	0.32	2.05	0.72	1.43		
		% of site	"C" Factor	Composite "C"			
<b>Open Water Area</b>		0.00	1.00	0.00			
<b>Impervious Area</b>		80.00	0.95	0.76			
<b>Pervious Area</b>		20.00	0.50	0.10			
<b>Total :</b>		<b>100.00</b>		<b>0.86</b>			

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Detention Calculator  
 Modified Rational Method

TELEPHONE (630) 774-9501			DESCRIPTION	Arlington Heights - BASIN CALCULATION SHEETS		
			Technical Bulletin 70 (7.58 in. - 100 Year Rainfall)			
			STORAGE VOLUME WITH ALLOWABLE RELEASE RATE-PHASE 1 BUILD-OUT			
DURATION (HOURS)	TIME (MIN)	100 YR. INT (IN/HR)	INFLOW RATE (CFS)	STORED RATE (CFS)	VOLUME (ACRE-FT)	
0.50	30	5.60	34.62	33.38	1.39	Area of site in acres: 6.93
0.67	40	4.92	30.41	29.17	1.62	Trapped water area in acres: 0.00
0.83	50	4.24	26.21	24.97	1.73	Net area for release computation in acres: 0.00
1.00	60	3.56	22.01	20.77	1.73	Allowable release rate in CFS: 1.24
1.50	90	2.90	17.93	16.69	2.09	Unrestricted release rate in CFS: 0.00
2.00	120	2.24	13.85	12.61	2.10	Bypass release rate in CFS: 0.00
3.00	180	1.62	10.01	8.77	2.19	Total allowable release in CFS: 1.24
4.00	240	1.40	8.63	7.39	2.46	Developed runoff coefficient: 0.89
5.00	300	1.17	7.25	6.01	2.51	Maximum volume in Acre-Ft = 2.55
6.00	360	0.95	5.87	4.63	2.32	
7.00	420	0.88	5.46	4.22	2.46	
8.00	480	0.82	5.05	3.81	2.54	
9.00	540	0.75	4.64	3.40	2.55 <====	
10.00	600	0.68	4.22	2.98	2.49	
11.00	660	0.62	3.81	2.57	2.36	
12.00	720	0.55	3.40	2.16	2.16	
13.00	780	0.52	3.24	2.00	2.16	
14.00	840	0.50	3.07	1.83	2.14	
15.00	900	0.47	2.91	1.67	2.08	Phase 1:
16.00	960	0.44	2.74	1.50	2.00	Total Tributary Area after development = 6.934 ac.
17.00	1020	0.42	2.58	1.34	1.89	Release rate = 1.24 cfs
18.00	1080	0.39	2.41	1.17	1.76	
19.00	1140	0.38	2.34	1.10	1.74	
20.00	1200	0.37	2.27	1.03	1.71	
21.00	1260	0.36	2.19	0.95	1.67	
22.00	1320	0.34	2.12	0.88	1.62	
23.00	1380	0.33	2.05	0.81	1.55	
24.00	1440	0.32	1.98	0.74	1.48	
	% of site	"C" Factor	Composite "C"			
Open Water Area	0.00	1.00	0.00			
Impervious Area	87.00	0.95	0.83			
Pervious Area	13.00	0.50	0.07			
<b>Total :</b>	<b>100.00</b>		<b>0.89</b>			

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Detention Calculator  
Modified Rational Method

TELEPHONE (630) 774-9501			DESCRIPTION		Arlington Heights - BASIN CALCULATION SHEETS		
					Technical Bulletin 70 (7.58 in. - 100 Year Rainfall)		
					STORAGE VOLUME WITH ALLOWABLE RELEASE RATE-PHASE 2		
DURATION (HOURS)	TIME (MIN)	100 YR. INT (IN/HR)	INFLOW RATE (CFS)	STORED RATE (CFS)	VOLUME (ACRE-FT)		
0.50	30	5.60	42.93	41.39	1.72	Area of site in acres:	8.56
0.67	40	4.92	37.72	36.18	2.01	Trapped water area in acres:	0.00
0.83	50	4.24	32.50	30.96	2.15	Net area for release computation in acres:	0.00
1.00	60	3.56	27.29	25.75	2.15	Allowable release rate in CFS:	1.54
1.50	90	2.90	22.23	20.69	2.59	Unrestricted release rate in CFS:	0.00
2.00	120	2.24	17.17	15.63	2.61	Bypass release rate in CFS:	0.00
3.00	180	1.62	12.42	10.88	2.72	Total allowable release in CFS:	1.54
4.00	240	1.40	10.71	9.17	3.06	Developed runoff coefficient:	0.90
5.00	300	1.17	8.99	7.45	3.11	Maximum volume in Acre-Ft =	3.16
6.00	360	0.95	7.28	5.74	2.87		
7.00	420	0.88	6.77	5.23	3.05		
8.00	480	0.82	6.26	4.72	3.15		
9.00	540	0.75	5.75	4.21	3.16	<==	
10.00	600	0.68	5.24	3.70	3.08		
11.00	660	0.62	4.73	3.19	2.92		
12.00	720	0.55	4.22	2.68	2.68		
13.00	780	0.52	4.01	2.47	2.68		
14.00	840	0.50	3.81	2.27	2.65		
15.00	900	0.47	3.60	2.06	2.58	Phase 2:	
16.00	960	0.44	3.40	1.86	2.48	Total Tributary Area after development = 8.556 ac.	
17.00	1020	0.42	3.19	1.65	2.34	Release rate = 1.54 cfs	
18.00	1080	0.39	2.99	1.45	2.17		
19.00	1140	0.38	2.90	1.36	2.15		
20.00	1200	0.37	2.81	1.27	2.12		
21.00	1260	0.36	2.72	1.18	2.07		
22.00	1320	0.34	2.63	1.09	2.00		
23.00	1380	0.33	2.54	1.00	1.92		
24.00	1440	0.32	2.45	0.91	1.83		
		% of site	"C" Factor	Composite "C"			
<b>Open Water Area</b>		0.00	1.00	0.00			
<b>Impervious Area</b>		88.00	0.95	0.84			
<b>Pervious Area</b>		12.00	0.50	0.06			
<b>Total :</b>		<b>100.00</b>		<b>0.90</b>			

**RWG ENGINEERING, LLC.**  
**975 E. 22nd Street**  
**Wheaton, IL 60189**  
**(630) 774-9501**

Detention Calculator  
Modified Rational Method

TELEPHONE (630) 774-9501			DESCRIPTION		Arlington Heights - BASIN CALCULATION SHEETS		
					Technical Bulletin 70 (7.58 in. - 100 Year Rainfall)		
					<b>STORAGE VOLUME WITH DESIGN RELEASE RATE-PHASE 1 TEMPORARY</b>		
DURATION	TIME	100 YR. INT	INFLOW RATE	STORED RATE	VOLUME	Area of site in acres:	7.44
(HOURS)	(MIN)	(IN/HR)	(CFS)	(CFS)	(ACRE-FT)	Trapped water area in acres:	0.00
0.50	30	5.60	35.81	34.60	1.44	Net area for release computation in acres:	0.00
0.67	40	4.92	31.46	30.25	1.68	Design release rate in CFS:	1.21
0.83	50	4.24	27.11	25.90	1.80	Unrestricted release rate in CFS:	0.00
1.00	60	3.56	22.77	21.56	1.80	Bypass release rate in CFS:	0.00
1.50	90	2.90	18.55	17.34	2.17	Total allowable release in CFS:	1.21
2.00	120	2.24	14.32	13.11	2.19	Developed runoff coefficient:	0.86
3.00	180	1.62	10.36	9.15	2.29		
4.00	240	1.40	8.93	7.72	2.57		
5.00	300	1.17	7.50	6.29	2.62	<b>Maximum volume in Acre-Ft =</b>	<b>2.69</b>
6.00	360	0.95	6.08	4.87	2.43		
7.00	420	0.88	5.65	4.44	2.59		
8.00	480	0.82	5.22	4.01	2.68		
9.00	540	0.75	4.80	3.59	2.69	<====	
10.00	600	0.68	4.37	3.16	2.63		
11.00	660	0.62	3.94	2.73	2.51		
12.00	720	0.55	3.52	2.31	2.31		
13.00	780	0.52	3.35	2.14	2.31		
14.00	840	0.50	3.18	1.97	2.29		
15.00	900	0.47	3.01	1.80	2.24	Phase 1:	
16.00	960	0.44	2.84	1.63	2.17	Total Tributary Area after Phase 1 = 7.436 ac.	
17.00	1020	0.42	2.66	1.45	2.06	Release rate = 1.21 cfs	
18.00	1080	0.39	2.49	1.28	1.93		
19.00	1140	0.38	2.42	1.21	1.91		
20.00	1200	0.37	2.34	1.13	1.89		
21.00	1260	0.36	2.27	1.06	1.86		
22.00	1320	0.34	2.20	0.99	1.81		
23.00	1380	0.33	2.12	0.91	1.75		
24.00	1440	0.32	2.05	0.84	1.67		
		% of site	"C" Factor	Composite "C"			
<b>Open Water Area</b>		0.00	1.00	0.00			
<b>Impervious Area</b>		80.00	0.95	0.76			
<b>Pervious Area</b>		20.00	0.50	0.10			
<b>Total :</b>		<b>100.00</b>		<b>0.86</b>			

**RWG ENGINEERING, LLC.**  
**975 E. 22nd Street**  
**Wheaton, IL 60189**  
**(630) 774-9501**

Detention Calculator  
Modified Rational Method

TELEPHONE (630) 774-9501			DESCRIPTION		Arlington Heights - BASIN CALCULATION SHEETS		
					Technical Bulletin 70 (7.58 in. - 100 Year Rainfall)		
					STORAGE VOLUME WITH DESIGN RELEASE RATE-PHASE 1 BUILD-OUT		
DURATION (HOURS)	TIME (MIN)	100 YR. INT (IN/HR)	INFLOW RATE (CFS)	STORED RATE (CFS)	VOLUME (ACRE-FT)	Area of site in acres:	6.93
0.50	30	5.60	34.62	33.41	1.39	Trapped water area in acres:	0.00
0.67	40	4.92	30.41	29.20	1.62	Net area for release computation in acres:	0.00
0.83	50	4.24	26.21	25.00	1.74	Design release rate in CFS:	1.21
1.00	60	3.56	22.01	20.80	1.73	Unrestricted release rate in CFS:	0.00
1.50	90	2.90	17.93	16.72	2.09	Bypass release rate in CFS:	0.00
2.00	120	2.24	13.85	12.64	2.11	Total allowable release in CFS:	1.21
3.00	180	1.62	10.01	8.80	2.20	Developed runoff coefficient:	0.89
4.00	240	1.40	8.63	7.42	2.47		
5.00	300	1.17	7.25	6.04	2.52	Maximum volume in Acre-Ft =	2.57
6.00	360	0.95	5.87	4.66	2.33		
7.00	420	0.88	5.46	4.25	2.48		
8.00	480	0.82	5.05	3.84	2.56		
9.00	540	0.75	4.64	3.43	2.57	<====	
10.00	600	0.68	4.22	3.01	2.51		
11.00	660	0.62	3.81	2.60	2.39		
12.00	720	0.55	3.40	2.19	2.19		
13.00	780	0.52	3.24	2.03	2.19		
14.00	840	0.50	3.07	1.86	2.17		
15.00	900	0.47	2.91	1.70	2.12	Phase 1:	
16.00	960	0.44	2.74	1.53	2.04	Total Tributary Area after development = 6.934 ac.	
17.00	1020	0.42	2.58	1.37	1.93	Release rate = 1.21 cfs	
18.00	1080	0.39	2.41	1.20	1.80		
19.00	1140	0.38	2.34	1.13	1.79		
20.00	1200	0.37	2.27	1.06	1.76		
21.00	1260	0.36	2.19	0.98	1.72		
22.00	1320	0.34	2.12	0.91	1.67		
23.00	1380	0.33	2.05	0.84	1.61		
24.00	1440	0.32	1.98	0.77	1.54		
		% of site	"C" Factor	Composite "C"			
<b>Open Water Area</b>		0.00	1.00	0.00			
<b>Impervious Area</b>		87.00	0.95	0.83			
<b>Pervious Area</b>		13.00	0.50	0.07			
<b>Total :</b>		<b>100.00</b>		<b>0.89</b>			

**RWG ENGINEERING, LLC.**  
**975 E. 22nd Street**  
**Wheaton, IL 60189**  
**(630) 774-9501**

Detention Calculator  
 Modified Rational Method

TELEPHONE (630) 774-9501			DESCRIPTION		Arlington Heights - BASIN CALCULATION SHEETS	
					Technical Bulletin 70 (7.58 in. - 100 Year Rainfall)	
<b>STORAGE VOLUME WITH DESIGN RELEASE RATE-PHASE 2</b>						
DURATION (HOURS)	TIME (MIN)	100 YR. INT (IN/HR)	INFLOW RATE (CFS)	STORED RATE (CFS)	VOLUME (ACRE-FT)	
0.50	30	5.60	42.93	41.40	1.73	Area of site in acres: 8.56
0.67	40	4.92	37.72	36.19	2.01	Trapped water area in acres: 0.00
0.83	50	4.24	32.50	30.97	2.15	Net area for release computation in acres: 0.00
1.00	60	3.56	27.29	25.76	2.15	Design release rate in CFS: 1.53
1.50	90	2.90	22.23	20.70	2.59	Unrestricted release rate in CFS: 0.00
2.00	120	2.24	17.17	15.64	2.61	Bypass release rate in CFS: 0.00
3.00	180	1.62	12.42	10.89	2.72	Total allowable release in CFS: 1.53
4.00	240	1.40	10.71	9.18	3.06	Developed runoff coefficient: 0.90
5.00	300	1.17	8.99	7.46	3.11	<b>Maximum volume in Acre-Ft = 3.16</b>
6.00	360	0.95	7.28	5.75	2.88	
7.00	420	0.88	6.77	5.24	3.06	
8.00	480	0.82	6.26	4.73	3.15	
9.00	540	0.75	5.75	4.22	3.16 <==	
10.00	600	0.68	5.24	3.71	3.09	
11.00	660	0.62	4.73	3.20	2.93	
12.00	720	0.55	4.22	2.69	2.69	
13.00	780	0.52	4.01	2.48	2.69	
14.00	840	0.50	3.81	2.28	2.66	
15.00	900	0.47	3.60	2.07	2.59	Phase 2:
16.00	960	0.44	3.40	1.87	2.49	Total Tributary Area after development = 8.556 ac.
17.00	1020	0.42	3.19	1.66	2.36	Release rate = 1.53 cfs
18.00	1080	0.39	2.99	1.46	2.19	
19.00	1140	0.38	2.90	1.37	2.17	
20.00	1200	0.37	2.81	1.28	2.13	
21.00	1260	0.36	2.72	1.19	2.09	
22.00	1320	0.34	2.63	1.10	2.02	
23.00	1380	0.33	2.54	1.01	1.94	
24.00	1440	0.32	2.45	0.92	1.85	
<hr/>						
	% of site	"C" Factor	Composite "C"			
Open Water Area	0.00	1.00	0.00			
Impervious Area	88.00	0.95	0.84			
Pervious Area	12.00	0.50	0.06			
Total :	100.00		0.90			

## Runoff Curve Number

Project: Phase 1 - Final  
Location: Arlington Heights, Cook County, IL  
File: CN 101217.xlsx

By: mrm Date: 10/12/2017  
Checked: mrm Date: 10/12/2017

Circle One: Present Developed Description: 7.436-Acre Site - Phase 1 - temp cond

$$CN \text{ (weighted)} = \frac{\text{total product}}{\text{total area}} = \frac{692.02}{7.436} = 93.063$$

Use CN = **93**

## RUNOFF CURVE NUMBER ADJUSTMENT CALCULATOR

### Site Information:

Total Site Area,  $A_w$  (ac) =

Runoff, R (in) =

P = rainfall depth (in) =

CN =

S =

Runoff Volume Over Watershed,  $V_w$  (ac-ft) =

Total Impervious Area,  $A_i$  (ac) =

### Volume of GI Provided:

Volume Control Storage,  $V_R$  =  ac-ft

1" of volume over impervious area  
Additional volume over the required 1"

Additional Volume,  $V_{GI}$  =  ac-ft

### Adjusted Volume Over Watershed, $V_{ADJ} = V_w - V_R - V_{GI}$

$V_{ADJ}$  (ac-ft) =

Adjusted Runoff Over Watershed,  $R_{ADJ} = \frac{V_{ADJ}}{A_w}$

$R_{ADJ}$  (in) =

$S_{ADJ}$  =

Adjusted CN for detention calc's,  $CN_{ADJ}$  =

\*Blue values are entered by user

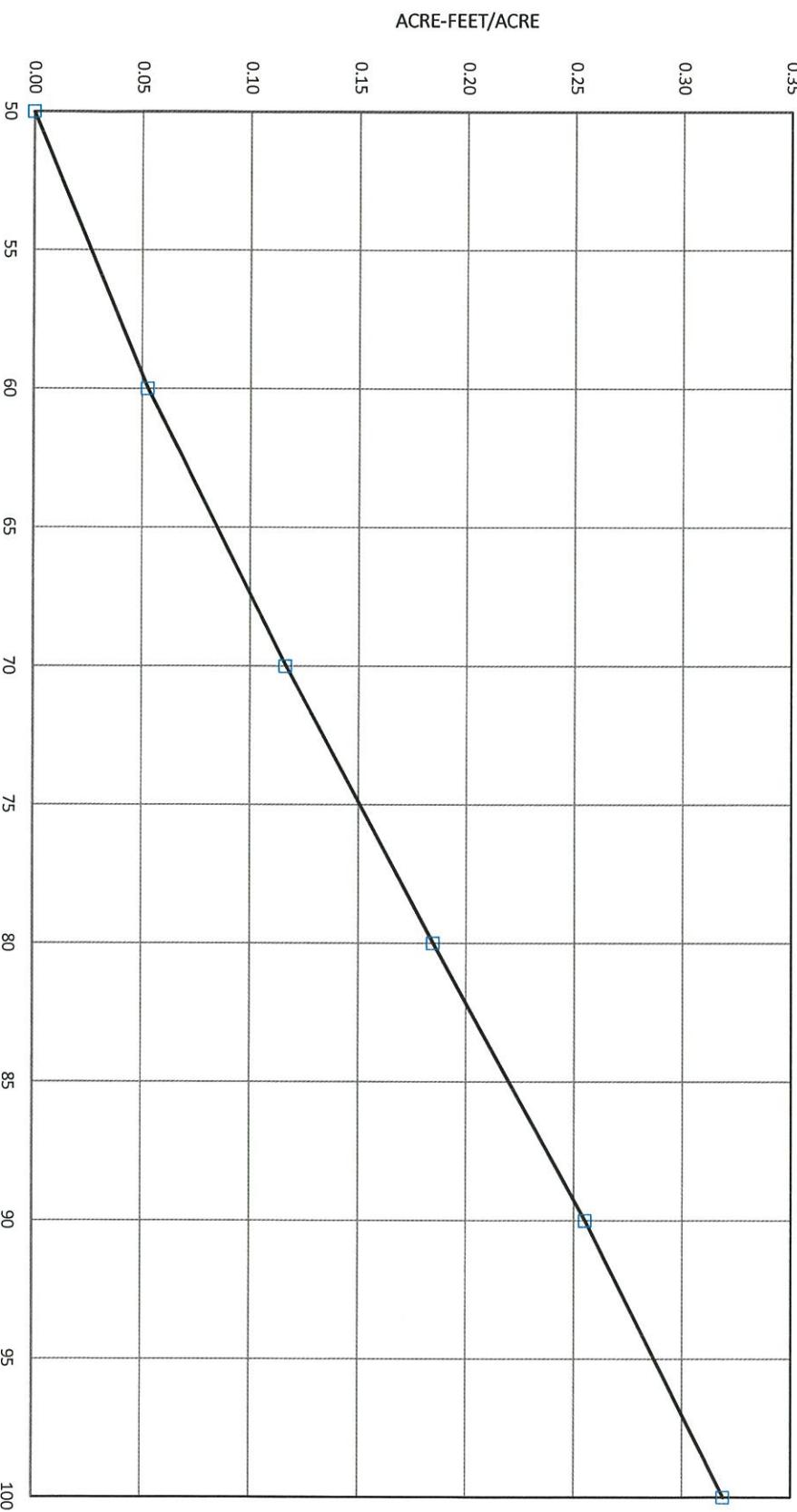
Enter Site Area:  acres

\*Blue Values are entered by user

Enter Reduced Curve Number for Site:

Estimated Required Detention Volume:  acre-feet

### DETENTION VOLUME VS REDUCED CURVE NUMBER\*



\*ADJUSTED FOR VOLUME CONTROL STORAGE PROVIDED, BASED ON RELEASE RATE OF 0.30 CFS/ACRE

## Runoff Curve Number

Project: Phase 1 - Final  
Location: Arlington Heights, Cook County, IL  
File: CN 101217.xlsx

By: mrm  
Checked: mrm

Date: 10/12/2017  
Date: 10/12/2017

Circle One: Present Developed Description: 6.934-Acre Site - Phase 1 - build out

$$CN \text{ (weighted)} = \frac{\text{total product}}{\text{total area}} = \frac{657.608}{6.934} = 94.838$$

Use CN = **95**

## RUNOFF CURVE NUMBER ADJUSTMENT CALCULATOR

### Site Information:

Total Site Area,  $A_w$  (ac) =

Runoff,  $R$  (in) =

$P$  = rainfall depth (in) =

CN =

S =

Runoff Volume Over Watershed,  $V_w$  (ac-ft) =

### Volume of GI Provided:

Volume Control Storage,  $V_R$  =  ac-ft

1" of volume over impervious area

Additional Volume,  $V_{GI}$  =  ac-ft

Additional volume over the required 1"

### Adjusted Volume Over Watershed, $V_{ADJ} = V_w - V_R - V_{GI}$

$V_{ADJ}$  (ac-ft) =

Adjusted Runoff Over Watershed,  $R_{ADJ} = \frac{V_{ADJ}}{A_w}$

$R_{ADJ}$  (in) =

$S_{ADJ}$  =

Adjusted CN for detention calc's,  $CN_{ADJ}$  =

Total Impervious Area,  $A_i$  (ac) =

\*Blue values are entered by user

Enter Site Area:  acres

\* Blue Values are entered by user

Enter Reduced Curve Number for Site:

Estimated Required Detention Volume:  acre-feet

### DETENTION VOLUME VS REDUCED CURVE NUMBER\*



\*ADJUSTED FOR VOLUME CONTROL STORAGE PROVIDED, BASED ON RELEASE RATE OF 0.30 CFS/ACRE

## Runoff Curve Number

Project: Phase 2 - Final  
Location: Arlington Heights, Cook County, IL  
File: CN 101217.xlsx

By: mrm Date: 10/12/2017  
Checked: mrm Date: 10/12/2017

Circle One: Present Developed Description: 8.556-Acre Site - Phase 2 - build out

$$CN \text{ (weighted)} = \frac{\text{total product}}{\text{total area}} = \frac{813.48}{8.556} = 95.077$$

Use CN = **95**

## RUNOFF CURVE NUMBER ADJUSTMENT CALCULATOR

### Site Information:

Total Site Area,  $A_w$  (ac) =

Runoff, R (in) =

P = rainfall depth (in) =

CN =

S =

Runoff Volume Over Watershed,  $V_w$  (ac-ft) =

Total Impervious Area,  $A_i$  (ac) =

### Volume of GI Provided:

Volume Control Storage,  $V_R$  =  ac-ft

1" of volume over impervious area

Additional Volume,  $V_{GI}$  =  ac-ft

Additional volume over the required 1"

### Adjusted Volume Over Watershed, $V_{ADJ} = V_w \cdot V_R \cdot V_{GI}$

$V_{ADJ}$  (ac-ft) =

Adjusted Runoff Over Watershed,  $R_{ADJ} = \frac{V_{ADJ}}{A_w}$

$R_{ADJ}$  (in) =

$S_{ADJ}$  =

Adjusted CN for detention calcs,  $CN_{ADJ}$  =

\*Blue values are entered by user

Enter Site Area:  acres

\* Blue Values are entered by user

Enter Reduced Curve Number for Site:

Estimated Required Detention Volume:  acre-feet

### DETENTION VOLUME VS REDUCED CURVE NUMBER\*



\*ADJUSTED FOR VOLUME CONTROL STORAGE PROVIDED, BASED ON RELEASE RATE OF 0.30 CFS/ACRE

**TABLE 2**  
**ARLINGTON HEIGHTS INDUSTRIAL**  
**SUMMARY OF STORMWATER STORAGE PROVIDED**

**PHASE 1 - NORTH**

<u>Basin</u>	<u>Description</u>	Det Storage (Ac-Ft)	Volume Control Storage (Ac-Ft)
N-1	Existing Pond	0.370	0
N-2	Modified Pond	1.115	0.095
N-3	Underground	0.500	0.400
N-4?	Truck Dock Area	0.579	0
	Pipe Storage	<u>0.117</u>	<u>0</u>
	Total Volume:	2.681	0.495

**PHASE 2 - SOUTH**

<u>Basin</u>	<u>Description</u>	Det Storage (Ac-Ft)	Volume Control Storage (Ac-Ft)
S-1	New Pond	0.704	0.049
S-2	Underground-W	0.938	0.429
S-3	Underground-SE	0.286	0.051
S-4	Underground-E	0.226	0.041
	Truck Dock Area	0.953	0
	Pipe Storage	<u>0.101</u>	<u>0</u>
	Total Volume:	3.208	0.569

# Cut/Fill Report -- STORAGE VOLUMES PROVIDED

**Generated:** 2017-10-18 09:59:53

**By user:** RWGENGSTA07

**Drawing:** S:\32212717 - HP Arlington Heights Industrial\300\_Engineering\310\_CADD\Exhibits\S:\32212717 - HP Arlington Heights Industrial\300\_Engineering\310\_CADD\Exhibits\322\_BASE\_Basin.dwg

Volume Summary							
Name	Type	Cut Factor	Fill Factor	2d Area (Sq. Ft.)	Cut (Cu. Yd.)	Fill (Cu. Yd.)	Net (Cu. Yd.)
EX Basin N-1 (Det) NWL 710.65	full	0.000	1.000	4405.29	0.00*	597.51	597.51*
Basin N-2 (Det) NWL 710.2	full	0.000	1.000	12790.21	0.00*	1798.88	1798.88*
Basin N-2 (Vol Control)	full	0.000	1.000	5316.58	0.00*	152.88	152.88*
North Truck Dock	full	0.000	1.000	52639.96	0.00*	934.61	934.61*
Basin S-1 (Det) NWL 709.8	full	0.000	1.000	9218.35	0.00*	1134.98	1134.98*
Basin S-1 (Vol Control)	full	0.000	1.000	3112.46	0.00*	78.87	78.87*
South Truck Dock	full	0.000	1.000	85783.42	0.00*	1537.32	1537.32*

Totals					
		2d Area (Sq. Ft.)	Cut (Cu. Yd.)	Fill (Cu. Yd.)	Net (Cu. Yd.)
Total		173266.27	0.00*	6235.04	6235.04*

\* Value adjusted by cut or fill factor other than 1.0

No. 322-127-17

12-Oct-17

ARLINGTON HEIGHTS INDUSTRIAL  
DETENTION STORAGE IN STORM SEWER SYSTEM  
BELOW 715.4 HWL

PHASE 1 - NORTH

Pipe Storage:

Pipe Size <u>(Inches)</u>	Length <u>(Feet)</u>	Area <u>(Sq Ft)</u>	Volume <u>(Cu Ft)</u>
10	284	0.545	154.819
12	353	0.785	277.105
15	334	1.227	409.672
18	535	1.766	944.944
21	191	2.404	459.176
24	348	3.140	1092.720
30	0	4.906	0.000
36	251	7.065	<u>1773.315</u>

Total Pipe Storage: 5111.751 0.117 Ac-Ft

PHASE 2 - SOUTH

Pipe Storage:

Pipe Size <u>(Inches)</u>	Length <u>(Feet)</u>	Area <u>(Sq Ft)</u>	Volume <u>(Cu Ft)</u>
10	302	0.545	164.632
12	301.5	0.785	236.678
15	325	1.227	398.633
18	341	1.766	602.291
21	0	2.404	0.000
24	182	3.140	571.480
30	405	4.906	1987.031
36	60	7.065	<u>423.900</u>

Total Pipe Storage: 4384.645 0.101 Ac-Ft

## WEIR FLOW CALCULATIONS ARLINGTON HEIGHTS INDUSTRIAL

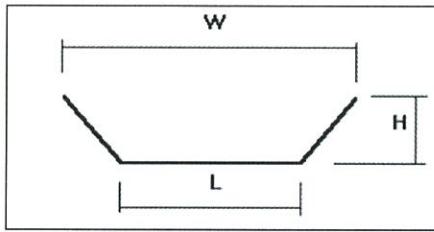
Designer:	PDL
Description:	100 YEAR-PHASE 1

BASED ON THE FOLLOWING EQUATION:

$$Q = \left[ K \times 2/3 \times L \times (2g)^{0.5} \times H^{1.5} \right] + \frac{1}{2} \left[ K \times 8/15 \times (2g)^{0.5} \times S_1 \times H^{2.5} \right] + \frac{1}{2} \left[ K \times 8/15 \times (2g)^{0.5} \times S_2 \times H^{2.5} \right]$$

WHERE:

Q = DISCHARGE IN CFS  
K = WEIR COEFFICIENT  
L = LENGTH IN FEET  
g = 32.2 FT/SEC  
H = HEAD IN FEET  
S<sub>1</sub> = LEFT SIDE SLOPE  
S<sub>2</sub> = RIGHT SIDE SLOPE



---

WEIR DATA: OVERFLOW CHANNEL AA-AA

- |                                |      |      |
|--------------------------------|------|------|
| 1. LENGTH, L                   | 26.0 | FEET |
| 2. WEIR COEFFICIENT, K (K<1.0) | 0.57 |      |
| 3. LEFT SIDE SLOPE, S (H:V)    | 1    | : 1  |
| 4. RIGHT SIDE SLOPE, S (H:V)   | 1    | : 1  |

5 RATING TABLE	HEAD (FEET)	DISCHARGE (CFS)
	0.20	7.14
	0.25	9.99
	0.30	13.15
	0.35	16.59
	0.40	20.31
	0.45	24.27
	0.50	28.46
	0.55	32.89
	0.60	37.53
	0.65	42.38

## WEIR FLOW CALCULATIONS ARLINGTON HEIGHTS INDUSTRIAL

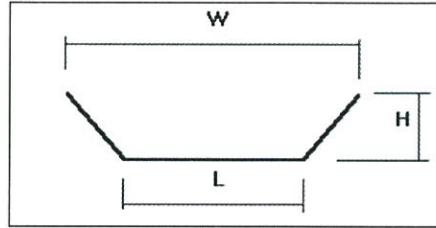
Designer:	PDL
Description:	100 YEAR-PHASE 2

BASED ON THE FOLLOWING EQUATION:

$$Q = \left[ K \times 2/3 \times L \times (2g)^{0.5} \times H^{1.5} \right] + \frac{1}{2} \left[ K \times 8/15 \times (2g)^{0.5} \times S_1 \times H^{2.5} \right] + \frac{1}{2} \left[ K \times 8/15 \times (2g)^{0.5} \times S_2 \times H^{2.5} \right]$$

WHERE:

Q = DISCHARGE IN CFS  
 K = WEIR COEFFICIENT  
 L = LENGTH IN FEET  
 g = 32.2 FT/SEC  
 H = HEAD IN FEET  
 S<sub>1</sub> = LEFT SIDE SLOPE  
 S<sub>2</sub> = RIGHT SIDE SLOPE




---

WEIR DATA: OVERFLOW CHANNEL AA-AA

1. LENGTH, L	20.0	FEET
2. WEIR COEFFICIENT, K (K<1.0)	0.50	
3. LEFT SIDE SLOPE, S (H:V)	1	: 4
4. RIGHT SIDE SLOPE, S (H:V)	1	: 4

5 RATING TABLE	HEAD (FEET)	DISCHARGE (CFS)
	0.30	8.90
	0.35	11.23
	0.40	13.75
	0.45	16.44
	0.50	19.29
	0.55	22.30
	0.60	25.46
	0.65	28.77
	0.70	32.21
	0.75	35.79
	0.80	39.51
	0.85	43.35
	0.90	47.32
	0.95	51.42
	1.00	55.64

## STORM SEWER WORKSHEET

Designer:	PDL	Date: 09-22-17
		Update: 10-12-17
Description:	PROPOSED ALGONQUIN ROAD INDUSTRIAL PARCEL-PH 1 (NORTH) ARLINGTON HEIGHTS, IL	

FREQUENCY: 10 YR.\* ROUGH. COEFF. 0.013 RUNOFF COEFF: Varies (See Below)

\* TYPICAL 10 YR FREQUENCY, EXCEPT RUN FROM EX STR 28 TO UNDERGROUND  
BASIN WHICH IS A 100 YEAR FREQUENCY-SEE BELOW

MH-MH	ADDED		TOTAL		C X A	TIME		I IN/HR	Q CFS	PIPE DIA IN	PIPE SLOPE %	VEL FPS	L FT	CAP CFS	COMMENTS
	"C" AC	AREA	"C" AC	AREA		FLOW MIN	T/C MIN								
<b>East Run</b>															
60-61	0.87	0.208	0.87	0.208	0.18	0.1	10.0	5.88	1.06	10.00	0.80	3.59	25	1.96	N13-Build-Out (Ph 2)
58-60	0.95	0.717	0.93	0.925	0.86	0.5	10.1	5.88	5.07	15.00	0.70	4.40	131	5.40	Add B8
56-58	0.85	0.201	0.92	1.126	1.03	0.5	10.6	5.88	6.07	18.00	0.40	3.76	122	6.64	N12/Str 59
54-56	0.84	0.153	0.91	1.279	1.16										N11/Str 57
	0.95	0.719	0.92	1.998	1.84	0.4	11.2	5.68	10.48	21.00	0.50	4.66	123	11.20	Add B7
Ex28-54	0.83	0.098	0.92	2.096	1.93	0.2	11.6	5.68	10.94	21.00	0.50	4.66	68	11.20	N10/Str 55
<b>Tributary Lateral Runs From South Curb Line</b>															
58-59	0.85	0.201	0.85	0.201	0.171	0.1	10.0	5.88	1.00	10.00	0.80	3.59	13	1.96	N12
56-57	0.84	0.153	0.84	0.153	0.129	0.1	10.0	5.88	0.76	10.00	0.80	3.59	13	1.96	N11
54-55	0.83	0.098	0.83	0.098	0.081	0.1	10.0	5.88	0.48	10.00	0.80	3.59	13	1.96	N10
62-63	0.78	0.093	0.78	0.093	0.073	0.1	10.0	5.88	0.43	10.00	1.25	4.49	16	2.45	N9
<b>North Parking Area-Restrictor MH to Basin N-2 -10 Year Frequency</b>															
Ex 28-62	0.92	2.096	0.92	2.096	1.93	0.1	11.6	5.68	10.94	36.00	0.03	1.63	10	11.55	From Str 54
62-64	0.77	0.093	0.91	2.189	2.00										N9
	0.95	0.261	0.92	2.450	2.25	0.6	11.7	5.68	12.75	36.00	0.04	1.89	70	13.34	Add B11
64-65	0.82	0.283	0.91	2.733	2.48	0.8	12.3	5.47	13.55	36.00	0.05	2.11	106	14.91	N8
65-68	0.84	0.186	0.90	2.919	2.63	0.5	13.2	5.26	13.85	24.00	0.38	4.44	128	13.95	N6
68-71	0.82	0.054	0.90	2.973	2.68										N4
	0.76	0.096	0.90	3.069	2.75	0.3	13.6	5.26	14.47	24.00	0.41	4.61	82	14.49	Add N1
71-70	0.93	0.088	0.90	3.157	2.83	0.2	13.9	5.26	14.90	24.00	0.44	4.78	51	15.01	N2
70-74	0.89	0.086	0.90	3.243	2.91	0.2	14.1	5.05	14.69	24.00	0.44	4.78	54	15.01	N3
74-73	0.95	0.073	0.90	3.316	2.98	0.1	14.3	5.05	15.04	24.00	0.45	4.83	33	15.18	Add B9
<b>North Parking Area-Restrictor MH to Basin N-3 -100 Year Frequency</b>															
Ex 28-62	0.92	2.096	0.92	2.096	1.93	0.1	11.6	9.66	18.60	36.00	0.08	2.67	10	18.86	From Str 54
62-64	0.77	0.093	0.91	2.189	2.00										N9
	0.95	0.261	0.92	2.450	2.25	0.4	11.7	9.66	21.69	36.00	0.11	3.13	70	22.12	Add B11
64-65	0.82	0.283	0.91	2.733	2.48	0.5	12.0	9.29	23.02	36.00	0.12	3.27	106	23.10	N8
65-66	0.84	0.186	0.90	2.919	2.63	0.3	12.6	9.29	24.47	36.00	0.13	3.40	65	24.05	N6
66-Basins	0.88	0.215	0.90	3.134	2.82										N7

Req'd H	Total H	Elev
0.003	1.517	713.72 OK, Rim @ 715.55
	1.514	713.71
0.028	1.514	713.71 OK, Rim @ 715.20
0.053	1.486	713.69
0.486	1.433	713.63 (Flow to Basin N-3 Begins at 713.41-
0.947	1.433	713.15 Would Reduce Flow To Basin N-2
0.336	0.947	713.15 Not Considered)
0.224	0.611	712.81
0.238	0.386	712.59
0.149	0.149	712.35 712.20 (Pipe Crown @ FES)

Req'd H	Total H	Elev
0.008	0.609	715.48 OK, Rim @ 715.55
	0.601	715.47
0.077	0.601	715.47 Rim @ 715.20 (Overflow @ 715.4)
0.127	0.524	715.39
0.085	0.397	715.27
0.313	0.313	715.18 714.87 Crown Basin N-3

FREQUENCY: 10 YR.\* ROUGH. COEFF. 0.013 RUNOFF COEFF: Varies (See Below)

\* TYPICAL 10 YR FREQUENCY, EXCEPT RUN FROM EX STR 28 TO UNDERGROUND  
BASIN WHICH IS A 100 YEAR FREQUENCY-SEE BELOW

Above worst case. Allowable/design release rate from site, as well as flow to Basin N-2 via 24" RCP not deducted from above flow review to Basin N-3

<u>Req'd H</u>	<u>Total H</u>	<u>Elev</u>	
0.140	2.202	713.90	OK, Rim @ 714.05
0.148	2.062	713.76	
0.000	1.914	713.61	
0.785	1.914	713.61	
	1.129	712.83	(Str 76 below)
0.016	1.646	713.35	
0.080	1.630	713.33	
0.040	1.550	713.25	
0.000	1.510	713.21	
0.146	1.510	713.21	

FREQUENCY: 10 YR.\* ROUGH. COEFF. 0.013 RUNOFF COEFF: Varies (See Below)

\* TYPICAL 10 YR FREQUENCY, EXCEPT RUN FROM EX STR 28 TO UNDERGROUND  
BASIN WHICH IS A 100 YEAR FREQUENCY-SEE BELOW

MH-MH	ADDED		TOTAL		C X A	TIME		I IN/HR	Q CFS	PIPE DIA IN	PIPE SLOPE %	VEL FPS	L FT	CAP CFS	COMMENTS
	"C" AC	AREA AC	"C" AC	AREA AC		FLOW MIN	T/C MIN								
76-77	0.92	0.210	0.94	1.236	1.17	0.3	11.9	5.68	6.63	18.00	0.40	3.76	59	6.64	N14
75-76	0.87	1.498	0.90	2.734	2.47	0.1	12.1	5.47	13.52	18.00	1.66	7.66	68	13.53	Add Run 76-86
Review Full Flow Velocity (Design Gradients) For Min 2.0 fps Velocity:															
										12.00	0.20	2.03		1.59	
										15.00	0.15	2.04		2.50	
										18.00	0.15	2.30		4.07	
										24.00	0.10	2.28		7.15	
										36.00	0.10	2.98		21.09	
Roof Drains															
B6	0.95	0.131	0.95	0.131	0.124	0.0	10.0	5.88	0.73	10.00	2.00	5.68	10	3.10	
B7	0.95	0.524	0.95	0.524	0.498	0.1	10.0	5.88	2.93	10.00	1.80	5.39	22	2.94	
B8	0.95	0.485	0.95	0.485	0.461	0.0	10.0	5.88	2.71	10.00	1.70	5.24	12	2.86	
B9	0.95	0.073	0.95	0.073	0.069	0.0	10.0	5.88	0.41	10.00	4.00	8.03	23	4.38	
B10	0.95	0.270	0.95	0.270	0.257	0.1	10.0	5.88	1.51	10.00	1.50	4.92	37	2.68	
B11	0.95	0.261	0.95	0.261	0.248	0.2	10.0	5.88	1.46	10.00	1.00	4.02	47	2.19	
B12	0.95	0.719	0.95	0.719	0.683	0.1	10.0	5.88	4.02	12.00	3.57	8.57	60	6.73	
B13	0.95	0.717	0.95	0.717	0.681	0.1	10.0	5.88	4.01	12.00	2.50	7.17	39	5.63	

0.236 1.365 713.06  
1.129 1.129 712.83 711.70 (Pipe Crown @FES)

## **STORM SEWER WORKSHEET**

Designer: Description: Phase 2 East Section

FREQUENCY: 10 YR.

ROUGH. COEFF. 0.013

RUNOFF COEFF: 0.50

tc	i
10	5.88
11	5.68
12	5.47
13	5.26
14	5.05
15	4.84
16	4.74
17	4.63
20	4.33

## STORM SEWER WORKSHEET

Designer:	
Description:	Phase 2 West Section

FREQUENCY: 10 YR.

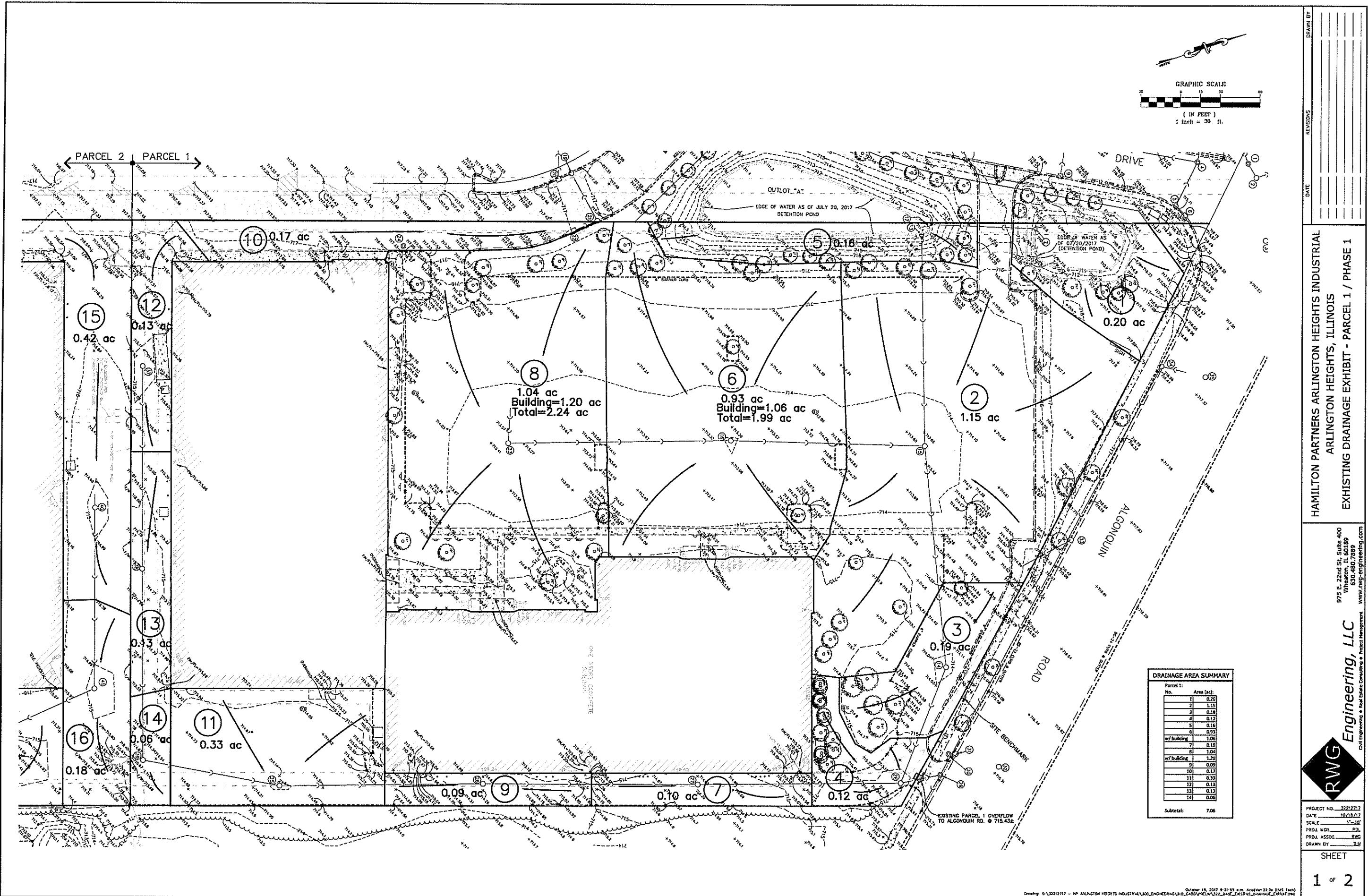
ROUGH. COEFF. 0.013

RUNOFF COEFF: 0.50

MH-MH	ADDED		TOTAL		C X A	TIME		I IN/HR	Q CFS	PIPE DIA IN	PIPE SLOPE %	VEL FPS	L FT	CAP CFS	UPPER MH			LOWER MH			COMMENTS
	"C" AC	AREA AC	"C" AC	AREA AC		FLOW MIN	T/C MIN								RIM	CROWN	INV	RIM	CROWN	INV	
87-88	0.87	0.230	0.87	0.230	0.200	0.2	10	5.88	1.18	10.00	0.30	2.20	26	1.20	714.05	711.98	711.15	714.05	711.90	711.07	
88-89	0.95	0.116	0.90	0.346	0.310	0.4	10.2	5.88	1.82	15.00	0.15	2.04	52	2.50	714.05	712.32	711.07	714.05	712.24	710.99	
89-90	0.95	0.117	0.91	0.463	0.421	0.3	10.6	5.88	2.48	15.00	0.15	2.04	39	2.50	714.05	712.24	710.99	714.05	712.18	710.93	
B5-90	0.95	0.524																			
90-91	0.95	0.134	0.93	1.121	1.047	0.3	10.9	5.88	6.15	18.00	0.35	3.52	72	6.21	714.05	712.34	710.84	715.69	712.09	710.59	
91-96	0.00	0.000	0.93	1.121	1.047			5.88	6.15	24.00	0.08	2.04	182	6.40	715.69	712.59	710.59	715.60	712.44	710.44	
92-93	0.95	0.117	0.95	0.117	0.111	0.3	10	5.88	0.65	10.00	0.25	2.01	39	1.10	714.05	711.98	711.15	714.05	711.88	711.05	
93-94	0.95	0.134	0.95	0.251	0.238	0.4	10.3	5.88	1.40	15.00	0.15	2.04	52	2.50	714.05	712.30	711.05	714.05	712.22	710.97	
94-95	0.95	0.117	0.95	0.368	0.350	0.3	10.7	5.88	2.06	15.00	0.15	2.04	39	2.50	714.05	712.22	710.97	714.05	712.16	710.91	
B4-95	0.95	0.524																			
95-96	0.95	0.134	0.95	1.026	0.975	0.4	11.1	5.68	5.54	18.00	0.28	3.15	72	5.56	714.05	712.34	710.84	715.60	712.14	710.64	
96-103	0.00	0.000	0.94	2.147	2.021	1.6	11.4	5.68	11.48	30.00	0.10	2.64	260	12.97	715.60	712.94	710.44	715.46	712.68	710.18	
97-98	0.95	0.115	0.95	0.115	0.109	0.3	10	5.88	0.64	10.00	0.25	2.01	39	1.10	714.05	711.98	711.15	714.05	711.88	711.05	
98-99	0.95	0.134	0.95	0.249	0.237	0.3	10.3	5.88	1.39	10.00	0.40	2.54	52	1.39	714.05	711.88	711.05	714.05	711.68	710.84	
99-100	0.95	0.117	0.95	0.366	0.348	0.3	10.7	5.88	2.04	15.00	0.15	2.04	39	2.50	714.05	712.09	710.84	714.05	712.03	710.78	
100-101	0.95	0.134	0.95	0.500	0.475	0.4	11.0	5.68	2.70	15.00	0.18	2.23	52	2.74	714.05	712.03	710.78	714.05	711.94	710.69	
B3-101	0.95	0.486																			
101-102	0.95	0.099	0.95	1.085	1.031	0.1	11.4	5.68	5.85	18.00	0.31	3.31	26	5.85	714.05	712.19	710.69	714.05	712.11	710.61	
102-103	0.89	0.269	0.94	1.354	1.270	0.3	11.5	5.68	7.21	18.00	0.48	4.12	72	7.28	714.05	712.11	710.61	715.46	711.76	710.26	
103-104	0.00	0.000	0.94	3.501	3.291	0.6	11.8	5.68	18.70	30.00	0.21	3.83	145	18.80	715.46	712.68	710.18	716.78	712.38	709.88	
105-104	0.95	0.082	0.95	0.082	0.078	0.3	10	5.88	0.46	10.00	0.25	2.01	39	1.10	715.88	713.71	712.88	716.78	713.62	712.78	
B1-104	0.95	0.073																			
104-V	0.00	0.000	0.94	3.656	3.439	0.3	12.4	5.47	18.81	36.00	0.13	3.40	60	24.05	716.78	712.88	709.88	N/A	712.80	709.80	

tc	i
10	5.88
11	5.68
12	5.47
13	5.26
14	5.05
15	4.84
16	4.74
17	4.63
20	4.33







**ARLINGTON HEIGHTS INDUSTRIAL  
ARLINGTON HEIGHTS, ILLINOIS  
PHASE 1 (NORTH) DRAINAGE AREA EXHIBIT**

975 E. 22nd St, Suite 400  
Wheaton, IL 60189  
630.480.7899  
[www.rwg-engineering.com](http://www.rwg-engineering.com)

RWG Engineering, LLC  
Civil Engineering • Real Estate Consulting • Project Management

PROJECT NO. 32212712  
DATE 09/22/17  
SCALE 1"=30'  
PROJ. MGR. PDL  
PROJ. ASSOC. RWG  
DRAWN BY AVS

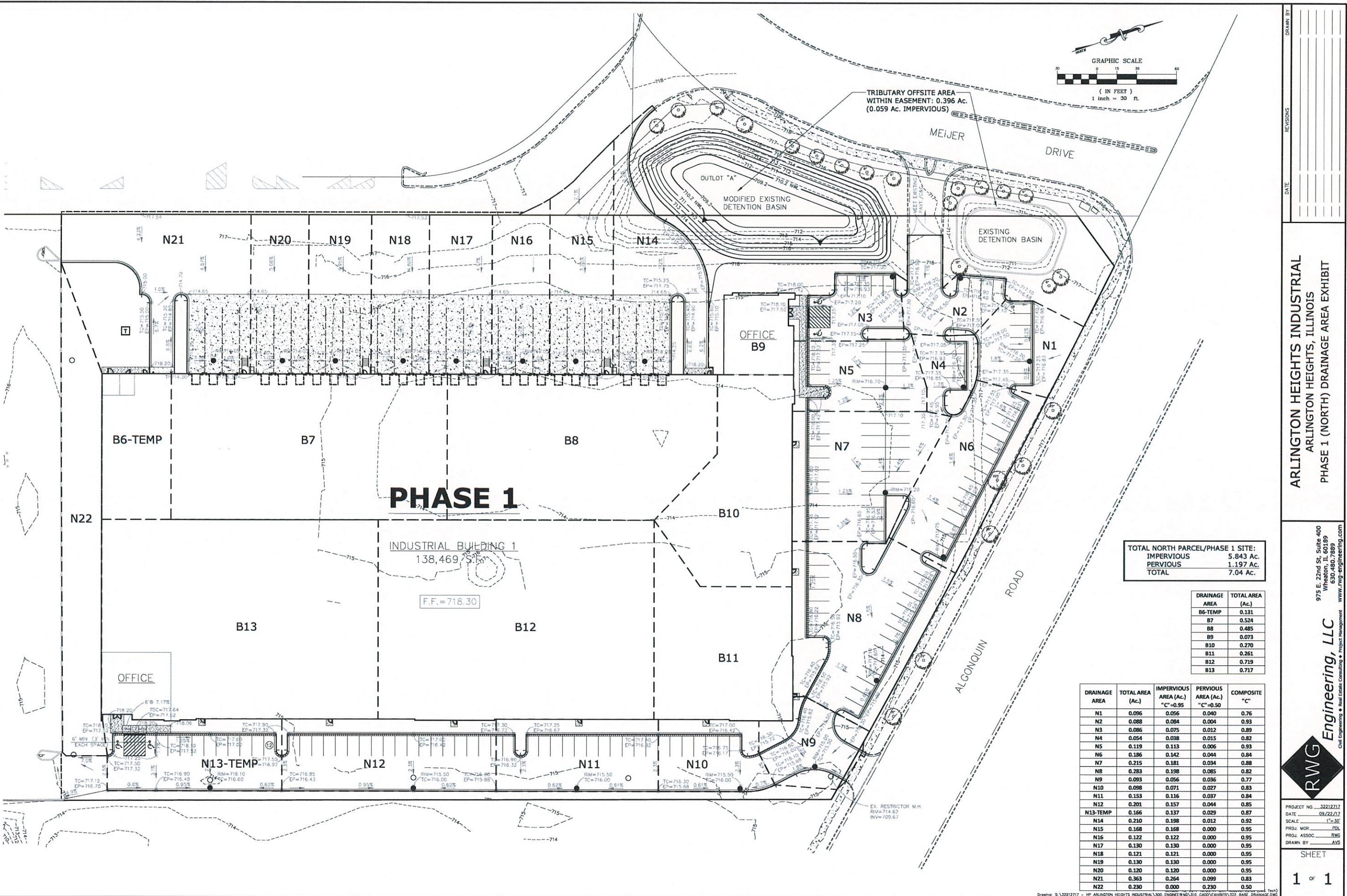
SHEET

1 OF 1

TOTAL NORTH PARCEL/PHASE 1 SITE:  
IMPERVIOUS 5.843 AC.  
Pervious 1.197 AC.  
TOTAL 7.04 AC.

DRAINAGE AREA	TOTAL AREA (AC.)
B6-TEMP	0.131
B7	0.524
B8	0.485
B9	0.073
B10	0.270
B11	0.261
B12	0.719
B13	0.717

DRAINAGE AREA	TOTAL AREA (AC.)	IMPERVIOUS AREA (AC.) "C"=0.95	PERVIOUS AREA (AC.) "C"=0.50	COMPOSITE "C"
N1	0.096	0.056	0.040	0.76
N2	0.088	0.084	0.004	0.93
N3	0.086	0.075	0.012	0.89
N4	0.054	0.036	0.015	0.82
N5	0.119	0.113	0.006	0.93
N6	0.186	0.142	0.044	0.84
N7	0.215	0.181	0.034	0.88
N8	0.283	0.198	0.085	0.82
N9	0.093	0.056	0.036	0.77
N10	0.098	0.071	0.027	0.83
N11	0.153	0.116	0.037	0.84
N12	0.201	0.157	0.044	0.85
N13-TEMP	0.166	0.137	0.029	0.87
N14	0.210	0.198	0.012	0.92
N15	0.168	0.168	0.000	0.95
N16	0.122	0.122	0.000	0.95
N17	0.130	0.130	0.000	0.95
N18	0.130	0.130	0.000	0.95
N19	0.120	0.120	0.000	0.95
N20	0.363	0.264	0.099	0.83
N21	0.230	0.000	0.230	0.50
N22	0.230	0.000	0.230	0.50



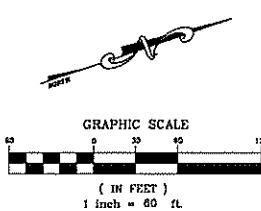
**ARLINGTON HEIGHTS INDUSTRIAL  
ARLINGTON HEIGHTS, ILLINOIS  
MASTER DRAINAGE AREA EXHIBIT**

RWG Engineering, LLC  
Civil Engineering • Real Estate Consulting • Project Management  
www.rwg-engineering.com

PROJECT NO. 22212217  
DATE 09/22/17  
SCALE 1"=40'  
PROJ. NO. B1 P1  
PROJ. ASSOC. B1  
DRAWN BY AIS

SHEET

1 OF 1



DRAINAGE AREA	TOTAL AREA (Ac.)	IMPERVIOUS AREA (Ac.) "C"=0.95	PERVIOUS AREA (Ac.) "C"=0.50	COMPOSITE "C"
N1	0.096	0.056	0.040	0.76
N2	0.088	0.084	0.004	0.93
N3	0.086	0.075	0.012	0.89
N4	0.054	0.038	0.015	0.82
N5	0.119	0.113	0.006	0.93
N6	0.186	0.142	0.044	0.84
N7	0.215	0.181	0.034	0.88
N8	0.283	0.198	0.085	0.82
N9	0.093	0.056	0.036	0.77
N10	0.098	0.071	0.027	0.83
N11	0.153	0.116	0.037	0.84
N12	0.201	0.157	0.044	0.85
N13	0.206	0.158	0.039	0.87
N14	0.210	0.198	0.012	0.92
N15	0.168	0.168	0.000	0.95
N16	0.122	0.122	0.000	0.95
N17	0.130	0.130	0.000	0.95
N18	0.121	0.121	0.000	0.95
N19	0.130	0.130	0.000	0.95
N20	0.120	0.120	0.000	0.95
N21	0.271	0.232	0.039	0.88

DRAINAGE AREA	TOTAL AREA (Ac.)
B1	0.073
B2	0.269
B3	0.486
B4	0.524
B5	0.524
B6	0.262
B7	0.524
B8	0.485
B9	0.073
B10	0.270
B11	0.261
B12	0.719
B13	0.717
B14	0.718
B15	0.719
B16	0.261

